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Speed Control of Brushless DC Motor Using Model Reference Adaptive Control

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ABSTRACT: Brushless DC motor drives are widely used in various industrial systems, such as servomotor drives, medical, automobile and aerospace industry. These are electronically commutated motor and offer many advantages over brushed DC motors which include increased efficiency, longer life, low volume and high torque. The main objective of the thesis is to design a controller to keep the output speed of the BLDC motor constant, under different operating conditions such as parameter variations, load disturbances etc. In model reference adaptive control, the plant output is varied with respect to the output of the reference model with some adjusting mechanism in order to obtain the speed control. The platform for modelling of BLDC motor and simulation of the control is MATLAB/Simulink

KEYWORDS: Brushless DC motors, PID Controller, Model Reference Adaptive Control, Lyapunov Stability Method.

I.INTRODUCTION

BRUSHLESS DC motors have wide industrial applications. These are used generally in servo, actuation, positioning and variablespeed applications where precise motion control is needed. They have been applied in the automotive, HVAC, electronics, computer, semiconductor and medical industries, BLDC motors have long been used in industrial applications such as actuators, feed drives for CNC machines, industrial robots, extruder drives. They are constructed in an inside out configuration with rotor having a set of permanent magnets and a stationary armature winding excited by an electronic commutation controller. The simple construction of BLDC motor has the advantage of high torque, low inertia and wide speed range. These motors exhibit better heat dissipation, improved efficiency, long life and greater power range. Due to lack of commutator and brushes their weight and size is reduced. The disadvantage of BLDC motors, brushes and commutators are absent. The commutation is done electronically by controlling the power switches that are used in the inverters of BLDC motors. Trapezoidal back emf and rectangular stator current are needed to produce a constant electric torque for such type of motors. The commutation region of back emf should be as small as possible so as to make it difficult to commutate a phase of that motor when driven by current source inverter. The flat portion of back emf should be 120° for constant torque production.

Scientists have made attempts to regulate the speed of motors for many years. Speed control using PWM (pulse width modulation) signals was one among the earlier techniques [1]. Feedback signals from the PMBLDC motor representing speed and position are utilized to get the driving signals for the inverter switches. It suppresses torque oscillations. It was more effective for low speed applications only.Conventional feedback controllers like proportional-derivative (PD) controllers and proportional-integral-derivative (PID) controllers were discussed to achieve speed control of BLDC motor [2]. The above mentioned techniques require accurate nonlinear model for better tracking. Soft computing techniques like Genetic algorithm were introduced. [3]Genetic Algorithm is proposed as a global optimizer to find optimized PID gains for position control of BLDC motor. It has a disadvantage of high power consumption. Using fuzzy logic as adesign methodology, which can be applied in developing nonlinear system for embedded control. Accommodates non-linearity without utilization of mathematical model developed the next controller [4].Speed



(An ISO 3297: 2007 Certified Organization)

Website: www.ijareeie.com

Vol. 6, Issue 5, May 2017

controllers using Fuzzy based PID controllers came into existence[5]. A single set of Fuzzy rules were used for controlling $k_{p}k_{i}$ and k_{d} values in the controller. It failed to adapt with change in parameters

In this paper a controller is designed to regulate the speed of BLDC motor using a conventional PID control technique and also a control technique with model reference adaptive control is used. A comparison of both these techniques are done based on the performance parameters like settling time and maximum overshoot.

The outline of this paper is as follows. Section II is the model description of BLDC motor; Section III involves the complete drive system for BLDC motor and Section IV is the design of controller to regulate the speed. The simulation results followed by its analysis is described in Section V Concluding remarks are given in Section VI.

II.SYSTEM MODEL

BLDC motor drive system consisting of BLDC motor and IGBT inverter is designed based on the assumptions that all stator phase windings are having same resistance per phase for stator windings; constant self and mutual inductances; ideal power semiconductor devices; negligible iron losses and motor is unsaturated.

The line to line voltages of BLDC motors in matrix form neglecting mutual inductances is given in (1)

V_{ab}	$\int R$	-R	$0 \left[i_a \right] \left[L \right]$	-L	$0] [i_a] [e_a - e_b]$	
$ V_{bc} =$	= 0	R	$-R \left i_{b} \right + 0$	L	$-L\left \frac{a}{dt}\right i_b \left +\right e_b - e_c$	(1)
V_{ca}	$\lfloor -R \rfloor$	0	$R \perp i_c \rfloor \ \lfloor -L$	0	$L \int at [i_c] [e_c - e_a]$	

where L is the mutual inductance ,R is the stator resistance per phase , e_a , e_b and e_c are back EMFs of phases a ,b and c respectively and i_a , i_b and i_c are the phase currents of phases a,b and c.

The electromagnetic torque developed by the motor is given by

$$T_e = (e_a i_a + e_b i_b + e_c i_c) \frac{1}{\omega} = k_t I$$
⁽²⁾

where $i_a = i_b = i_c = I$, ω is the angular velocity in radians per second and k_t is the torque constant.

Since this electromagnetic torque is used to overcome the opposing torques of inertia and load, it can be utilized to overcome the inertial and opposing torques of inertia, it can be written as

$$T_e = T_l + J_M \frac{d\omega}{dt} + B_M \omega \tag{3}$$

Where T_1 is the load torque, J_M is the inertial constant and B_M is the frictional constant.



Fig 1: Equivalent circuit of BLDC motor drive system



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Website: <u>www.ijareeie.com</u>

Vol. 6, Issue 5, May 2017

The transfer function model of BLDC motor is given by

$$G(s) = \frac{\omega(s)}{V(s)} = \frac{k_t}{s^2 JL + sRJ + k_e k_t}$$
(4)

Multiplying and dividing throughout the equation by $\frac{R}{k_e k_t} \times \frac{1}{R}$. Then Transfer function becomes,

$$G(s) = \frac{\omega(s)}{V(s)} = \frac{\frac{1}{k_e}}{\tau_m \tau_e s^2 + \tau_m s + 1}$$
(5)

Where $\tau_m = \sum \frac{RJ}{k_e k_t}$ is the mechanical time constant and $\tau_e = \sum \frac{L}{R}$ is the electrical time constant.

III.COMPLETE DRIVE SYSTEM

The fig:2 shows the complete block diagram showing the drive system of BLDC motor. Drive system includes the BLDC motor, inverter, controller and three Hall Effect sensors. Reference speed to which the motor is to be regulated is given as input to the controller. The rotor position is detected by using the three Hall Effect sensor signals and is fed back to the controller along with actual speed of BLDC motor. The controller generates the control signal based on the model reference adaptive control law which is used for speed regulation. These control signals are then converted to Pulse Width Modulated signal which are given to drive the inverter switches. The control signal varies the duty cycle of the pulses which are applied across the inverter switches. This controls the average voltage across the winding so that speed of the motor is varied.



Fig 2: Complete drive System



(An ISO 3297: 2007 Certified Organization)

Website: www.ijareeie.com

Vol. 6, Issue 5, May 2017

IV.CONTROLLER DESIGN

A. PID Controller

It has wide industrial applications as it need only less parameters to be tuned. It eliminates the steady state error by integral action and anticipates the change in output by derivative action. For tuning of parameters in PID controller a lot of techniques are available. Zeigler Nicholas Tuning method is the most popular method for tuning of PID controller. It depends mainly on step response of the system.

The continuous control signal u(t) of the system is given by,

$$u(t) = k_p \left(e(t) + \frac{1}{T_i} \int e(t) + T_d \frac{de(t)}{dt} \right)$$
(4)

Using Zeigler Nicholas method of tuning the parameters of the PID controller is given by kp=5.7748 ,ki=1605.29 and kd=0.00468.



Figure 3: Simulink block diagram of PID controller

B. Model Reference Adaptive Controller

Adaptive Control process is the one that continuously and automatically measures the dynamic behavior of plant, compares it with desired output and uses the difference to vary adjustable system parameters or to generate the actuating signal in such a way as to obtain optimal performance. An adaptive control system has two loops. One is the normal feedback with process and controller and the other loop consists of the adjustment loop. The parameter adjustment loop is often slower than the normal feedback loop. It can adapt to any change in the speed which occurs due to variation in load or due to external disturbances.

In model reference adaptive controller, controller is designed to force the system or plant to behave like reference model. Model output is compared to the actual output, and the difference is used to adjust the feedback controller parameters MRAS has two loops :inner loop an ordinary control loop consisting of plant and regulator, an outer loop or adaptation loop that adjust the control parameters in order to reduce the error between model and plant output to zero. Mathematical techniques like MIT rule and Lyapunov theory are used to develop adaptation mechanism in this paper.

i) MRAC based on MIT Rule

Consider a closed loop system in which the controller has one adjustable parameter θ . The desired closed loop response is specified by a model whose output is y_m . Let e be the error between the output y and output y_m . The control parameter is adjusted such that the loss function is minimized.



(An ISO 3297: 2007 Certified Organization)

Website: <u>www.ijareeie.com</u>

Vol. 6, Issue 5, May 2017

Loss function, $J = \frac{1}{2}e^2$ (5) In order to minimize the function, the control parameters should be changed in negative direction of the function.

$$\frac{\partial \theta}{\partial t} = -\gamma \frac{\partial F}{\partial \theta} = -\gamma e \frac{\partial e}{\partial \theta}$$
(6)

 $\frac{\partial e}{\partial \theta}$ is called the sensitivity derivative of the system.

A critically damped second order system is chosen as reference model with damping ratio as 1 and natural frequency as 1000 whose transfer function is given by

$$G_m(s) = \frac{B_m}{A_m} = \frac{1000000}{s^2 + 2000 s + 1000000}$$
(7)

The control law is chosen as

$$u = Tu_c(t) - Sy(t) \tag{8}$$

where $T = \frac{b_m}{b}$ and $S = \frac{a_m - a}{b}$ are the controller polynomials and $u_c(t)$ is the desired speed of the motor.

The update rule for controller parameter using MIT rule is described by

$$\frac{dT}{dt} = -\gamma \frac{bu_c}{s+a_m} e$$

$$\frac{dS}{dt} = -\gamma \frac{by}{s+a_m} e$$
(9)



Figure 4: Simulink model of Model Reference Adaptive Controller using MIT rule

ii) MRAC with Lyapunov Stability Method

Model Reference Adaptive control with Lyapunov Stability method is generally used for first and second order systems. An advantage of this method is that a different adaptation law is not required even if we change the reference model or the plant, unless the performance seems to be insufficient. The Lyapunov method attempts to find the Lyapunov function and an adaptation mechanism such a way that the error between plant and model goes to zero. Also this method ensure stability to the system.



(12)

(13)

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(An ISO 3297: 2007 Certified Organization)

Website: <u>www.ijareeie.com</u>

Vol. 6, Issue 5, May 2017

Let the reference model be given as a first order system

$$\frac{dy_m}{dt} = -a_m y_m + b_m u_c$$

Let the controller be

 $u(t) = \theta_1 u_c(t) - \theta_2 y(t)$ ⁽¹¹⁾

Error goes to zero when parameters,

$$\theta_1 = \frac{b_m}{b}$$
$$\theta_2 = \frac{a_m - a}{b}$$

The Lyapunov Function is taken as

$$V(e,\theta_1,\theta_2) = \frac{1}{2}(e^2 + \frac{1}{by}(b\theta_2 + a - a_m)^2 + \frac{1}{by}(b\theta_1 - b_m)^2)$$
(14)

According to Lyapunov, the system is said to be stable when dV/dt is negative definite. So in order to make the system stable the parameters are updated as

$$\frac{d \theta_1}{dt} = -\gamma u_c e$$

$$\frac{d \theta_2}{dt} = \gamma y e$$
(15)

Then the derivative dV/dt becomes $-a_me^2$ which is negative definite. Hence the system is stable.



Figure 6: Simulink model of Model Reference Adaptive Controller using Lyapunov Stability Method.

Adaptation gain γ is chosen as 0.00001 based on the performance analysis.



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Website: <u>www.ijareeie.com</u>

Vol. 6, Issue 5, May 2017

V. RESULT AND DISCUSSION

A Brushless motor drive system was modeled. Adaptive controller with MIT rule and Lyapunov Stability Method was designed and applied to the model and a compared with the results of the conventional PID controller. All the simulations were carried out in MATLAB/ Simulink. Step input was given as the reference to study the response of controller.Fig.5 shows the response of BLDC motor drive system without controller.

A.Response of PID controller

The controller parameters for the conventional PID controller are found such that it guarantees required tracking and also maintains the stability of the overall system. Zeigler Nicholas method of tuning is used to find the controller parameter which cope with the steady state error, overshoot and settling time requirements. The designed controller parameters are $k_p = 5.7748$, $k_i = 1605.29$, $k_d = 0.00468$ for speed tracking performance. The step responses of the PID controller for the system with variation in speed from 1000 rpm to 1500 rpm is shown in Fig. 6 and Fig.7 respectively High overshoot upto 3000 rpm is observed for the system. This can cause harm to the motor. In order to reduce overshoot the controller with Model Reference Adaptive control technique is designed.



: Response of PID controller

B. Response of Model Reference Adaptive control

The Model Reference Adaptive controller is designed as discussed in the above sections. Error between the reference speed and actual speed is forced to zero using adaptation mechanism. The responses of the system when MRAC with MIT rule is applied with variation of speed from 1000 rpm to 1500 rpm is shown in fig.9 For Adaptive controller with MIT rule we can see that the disturbances and overshoot are considerably reduced, thus reducing the steady state error and settling time. But have considerable overshoot.



Fig.8: Response of Model Reference Adaptive controller With MIT rule

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Vol. 6, Issue 5, May 2017



Fig.9 Response of Model reference Adaptive controller with Lyapunov Stability method

The model reference adaptive control using Lyapunov stability method shows considerably less overshoot and perfect tracking control with stability is ensured. Thus Model Reference Adaptive Control using Lyapunov Stability Method shows the best control performance as compared to PID controller. Only an overshoot of 6.7 % is observed.

 TABLE I

 Comparison between the characteristics of two controllers

Performance	PID	MRAS	with	MRAS With Lyapunov
Characteristics	controller	MIT rule		Stability Method
Maximum	81.2 %	17 %		6.7 %
Overshoot				
Settling time	0.05 s	0.8 s		0.2 s

TABLE II
Specifications of BLDC motor used for simulation

PARAMETERS	VALUES
Rated Power	6000W
Rated Voltage	315 V
Rated Current	20 A
Rated speed	1500 rpm
Rated Torque	30 Nm
Stator Resistance	0.43Ω
Stator inductance	0.00255H
Inertial Constant	0.0011
Viscous Friction	0.05
Coefficient	

VI.CONCLUSIONS

The model of BLDC motor is developed and a controller is designed using PID controller and Model Reference Adaptive controller algorithm with MIT rule as well as Lyapunov Stability method such that the speed control is obtained and is implemented using MATLAB/Simulink. A comparative study between these two techniques were undergone which shows that Model Reference Adaptive controller with Lyapunov Stability method shows better results as it reduces the maximum overshoot and also disturbances are reduced. There is considerable reduction in steady state error. The stability of the system is ensured using this type of controller.



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Website: www.ijareeie.com

Vol. 6, Issue 5, May 2017

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